MAY 15-18, 2017

PROGRAM GUIDE

COMBUSTION INSTITUTE CANADIAN SECTION



SPRING TECHNICAL MEETING 2017

MCGILL UNIVERSITY

General Information

Welcome to McGill University

The Alternative Fuels Laboratory at McGill University welcomes you to the Spring Technical Meeting of the Combustion Institute - Canadian Section (CICS 2017). The technical program includes three plenary lectures and approximately 80 presentations exposing the remarkable diversity of the combustion research performed in Canadian laboratories. The social program of CICS 2017 features a welcome reception on Monday evening at the McGill Faculty Club and a banquet, Wednesday evening, at the Érablière Charbonneau in Mont St-Grégoire where a traditional Québec meal will be served.

The CICS organizing committee wish you a pleasant stay in Montréal.

- Jeffrey M. Bergthorson, co-chair
- Gilles Bourque, co-chair
- Philippe Julien

Acknowledgements

We want to acknowledge the generous technical and financial support of our sponsors:

- Siemens Canada Limited,
- the Department of Mechanical Engineering, McGill University,
- the Faculty of Engineering, McGill University.

Thanks also to the students of the Alternative Fuels Laboratory for their help in organizing the meeting.

Welcome Reception

Participants are invited to a welcome reception on Monday May 15, starting at 6 pm. The event will be held at the McGill Faculty Club housed in a historic building on the campus (see map). Refreshments and hors d'oeuvres will be served.

Registration Desk and Information Table

The registration desk will be open:

- Monday, May 15 from 6 to 9 pm during the reception at the McGill Faculty Club,
- Tuesday, Wednesday, and Thursday, from 7:30 am to 5:00 pm, in McConnell 12.

Conference Banquet

The CICS Banquet will be held on Wednesday, May 17, at the Érablière Charbonneau in Mont St-Grégoire. A traditional Québec meal will be served at the cabane à sucre, along with maple syrup to accompany the dishes.

More information about the sugar shack and the menu can be found on the website. Buses will start loading at 6 pm on Wednesday at the location shown on the map. The last bus will depart at 6:30 pm.

Proceedings

Each registrant will receive a USB flash drive containing the proceedings. A link is embedded in the title of each paper in the program that will open the corresponding manuscript. For Adobe Acrobat Reader users, in order for the program not to close every time a paper is opened, uncheck the box *Open cross-document links in same window* under *Edit / Preferences / Documents*.

Wireless Internet Access

Wireless internet is available through Eduroam using your home institution's login information. For participants without access to Eduroam (outside of academia), individual username and password, valid for the duration of the meeting, can be obtained at the registration desk.

If further assistance is required, please contact the McGill IT Service Desk by email or call 514-398-3398.

Parking

Limited pay parking is available in the courtyard behind the McConnell Engineering Building. Parking is also possible behind the Percival Molson Memorial Stadium, or in the streets surrounding McGill University. Details can be found at: https://www.mcgill.ca/transport/parking/downtown/visitors.

Plenary Lectures and Technical Sessions

All conference talks will be presented in the McConnell Engineering Building (see map). Plenary lectures will be held in room McConnell 204, and technical sessions in rooms McConnell 11 (ground floor), McConnell 13 (ground floor), and McConnell 204 (second floor).

Instruction for Presentations

A computer (Windows operating system) and a projector are provided in each room. Each paper in the technical sessions has been allotted 20 minutes: 15 minutes for the presentation, 3 minutes for the question period, and 2 minutes for setup of the next presentation. Speakers are asked to bring their presentation on a USB flash drive and to upload it on the computer during the break preceding their session. Those using Apple computers are invited to test their presentation beforehand, or to bring their own computer along with the appropriate adapter to the VGA cable.

CICS 2017 will use the same computer timing system that has been utilized in previous meetings. The countdown clock will be green during the first 13 minutes of the presentation, then change to yellow at the end of the presentation and during the question period (next 5 minutes), and finally to red during the changeover (2 minutes). Please respect the time limit for your presentation.

Speakers should arrive at least 15 minutes before their session is scheduled to start in order to meet the Session Chair, and upload their presentation on the computer.

Coffee Breaks

Coffee breaks take place on Tuesday (morning and afternoon), Wednesday (morning and afternoon) and Thursday (morning) in room McConnell 12.

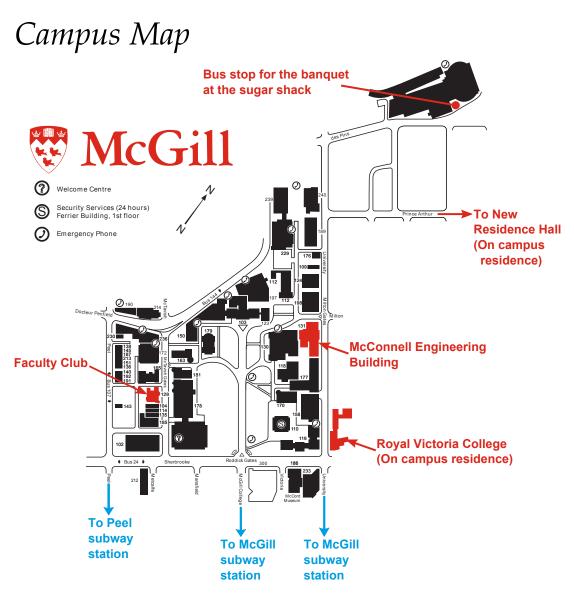
Lunch

Lunch is not provided with your registration. Many restaurants are at walking distance from the campus:

- Tim Hortons,
- Falafel Avenue,
- Vua,
- Les Trois Brasseurs,
- Lola Rosa Café (vegetarian restaurant),
- Amelias Pizza (closed on Monday),
- Second Cup,
- Numerous restaurants in the Eaton Center,
- and so on.

Facebook Page

A facebook page has been created for the CICS Spring Technical Meeting 2017. Please follow the page and share pictures of your work and taken during the conference! You can post your questions and comments on the wall.



Additional information about the campus and its neighbourhood is provided in this interactive map.

Program

Monday May 15, 2017

	15:30-18:00	Informal CICS Board Meeting (McGill Faculty Club / Gold Room)
ſ	18:00-21:00	Registration and Reception (McGill Faculty Club)

Tuesday May 16, 2017

7:30-8:00	30-8:00 On-site registration (McConnell 12)	
8:00-8:10	Welcome and Opening R	Remarks (McConnell 204)
	Plenary Lecture 1 (McConnell 204): Tailoring the Ignition and Combustion of	
	Aluminum in Propellants	
8:10-9:00	Prof. Steven F. Son, School of Mechanical Engineering	
	Purdue U	Jniversity
Chair: Jeffrey M. Bergthorson		M. Bergthorson
	McConnell 204	McConnell 11
	Heterogeneous and spray combustion	Pollutant formation
	Chair: John Z. Wen	Chair: Murray J. Thomson
	Effect of Nozzle Exit Conditions on the	Gas turbine emissions and contrail
	Near-Field Behavior of a Liquid Jet in a	microphysics at different operating
9:10-9:30	Uniform Cross Airflow M. Broumand and	conditions using complex chemistry and
	M. Birouk	microphysics J. Garcia Lopez, P. Seers,
		F. Garnier and X. Vancassel
	A Thermophysical Approach to the	Effect of different preparation and
0.30-0.20	Ignition of Particles M. Soo, X. Mi,	structure of Iron doped Cerium oxide
9:30-9:50	S. Goroshin, A.J. Higgins and J.M. Bergthorson	catalyst on soot combustion B. Li,
		H. Zheng, J.Z. Wen and E. Croiset
		The effect of pressure on the primary soot
	Evaporation of Droplets of Mixtures of	particle size in nitrogen diluted ethylene
0.50-10.10	n-Paraffins and n-Alkanols W. Hallett,	diffusion flames determined by
9:50-10:10	A. Tanner and N. McLellan	thermophoretic sampling at pressures up
		to 20 bar P.H. Joo, M. Christensen, E. Griffin,
		B. Gigone and Ö.L. Gülder

10:10-10:30	Reaction mechanism of layered Al/CuO nano-thermite composite <i>H. Sui and</i> <i>J.Z. Wen</i>	Thermochemical mechanism optimization for accurate predictions of CH concentrations in premixed flames of C1-C3 alkane fuel <i>P. Versailles,</i> <i>G.M.G. Watson, A. Durocher, G. Bourque and</i> <i>J.M. Bergthorson</i>
10:30-10:50	Coffee break ir	n McConnell 12
	New technology concepts Chair: Larry W. Kostiuk	IC and gas-turbine engine combustion Chair: Cécile Devaud
10:50-11:10	Hydrothermal Gasification of Biomass in Diamond Anvil Cell S. Nanda, A.K. Dalai, I.S. Butler and J.A. Kozinski	Chemical Imaging in a Diesel-Ignited Optical Engine Using High-Speed Infrared Narrowband Imaging M. Gagnon, E. Mancaruso, L. Sequino, P. Tremblay, S. Savary and V. Farley
11:10-11:30	The influence of empirical bed modeling on CO emissions in a small-scale grate firing biomass furnace Z. Taban, M. Farokhi and M. Birouk	Completness of Combustion in a Natural Gas Fueled Split-Cycle Engine S.G. Dal Bello and A. Sobiesiak
11:30-11:50	CFD analysis of a Variable Compression Ratio HCCI Rotary Engine <i>P. Panchal,</i> <i>G. Ciccarelli, P. Mottaghian and R. Fanara</i>	Flame liftoff and reattachment dynamics in a linear multi-swirler combustor array W.Y. Kwong and A.M. Steinberg
11:50-12:10	A novel method of calculating mass fraction of coated black carbon K.N. Broda, J.S. Olfert, M. Irwin, G. Schill, G. McMeeking, E. Schnitzler and W. Jäger	Study of the Promotion Effect of Hydrocarbon on NO-NO2 Conversion Process during Diesel Low-Temperature Combustion Cycles X. Yu, T. Gao, K. Xie, S. Yu and M. Zheng
12:10-12:30	Preliminary experimental study of methane decarbonization using a laminar premixed flame <i>F. Falahati, M.J. Afroughi,</i> <i>J.S. Olfert and L.W. Kostiuk</i>	Analysis of intermittent thermoacoustic oscillations in a liquid-fueled aeronautical gas turbine combustor at elevated pressure <i>S. Kheirkhah, J.M. Cirtwill,</i> <i>P. Saini, K. Venkatesan and A.M. Steinberg</i>

12:30-14:00	Lunch (On your own, see suggestion list)	
	Board of Directors Meeting (Macdonald 267)	
	McConnell 13	McConnell 11
	Laminar flames	Diagnostics
	Chair: W. Kendal Bushe	Chair: Mathieu Picard
	Evaluation of Maximum-Entropy Moment	Simultaneous laser Rayleigh and filtered
14:00-14:20	Closures for Predicting Radiation	laser Rayleigh scattering thermometry of
-4.00 -4.20	Transport Phenomena J.A.R. Sarr and	heated air K. Teav, N.E. Gowland and
	C.P.T. Groth	A.M. Steinberg
	Numerical Simulation of Laminar	Parametric study of effects of density
14:20-14:40	Diffusion Flames with an Aliphatic	ratio and fuel composition on coupled
14.20 14.40	Collision Inception Model N. Ceranic and	dynamics of hydrodynamic instability
	S.B. Dworkin	and flame lift-off Q. An and A.M. Steinberg
	Prediction of Laminar Diffusion Co-Flow	Assessment of Thermal Oxidation
14:40-15:00	Flames Coupled with Conjugate Heat	Stability Characteristics of Biojet Fuels
14.40 15.00	Transfer Using a Partitioned Approach	Using a New Technique N.G. Young,
	W. Syed and C.P.T. Groth	F.T.C. Yuen and Ö.L. Gülder
	Modeling soot formation with	Assessment of a Novel Optical Diagnostic
15:00-15:20	Flamelet-Generated-Manifold (FGM)	to Quantify Emissions from a Heated
19.00 19.20	method L. Zimmer, F.M. Pereira, J.A. van	Methane Plume S.J. Grauer, B.M. Conrad,
	Oijen and L.P.H. de Goey	R.B. Miguel and K.J. Daun
15:20-15:40	Coffee break in McConnell 12	
	McConnell 13	McConnell 11
	Turbulent flames	Detonations, explosions, and supersonic
	furbulent numes	combustion
	Chair: Clinton P.T. Groth	Chair: Gaby Ciccarelli
		Visualization of Detonation Propagation
15:40-16:00	Large Eddy Simulation of turbulent lifted	in a Round Tube Equipped with
15.40-10.00	flame M. Mortada and C. Devaud	Repeating Orifice Plates G. Rainsford and
		G. Ciccarelli
	Effect of Burner Geometry and Swirl	Dynamics of 2H2/O2/2Ar Detonations in
16:00-16:20	Strength on the Blowoff Limit of Lean	Channels with Constant Area Divergence
10.00-10.20	Premixed Biogas Flame A. Al-Abbasi,	Q. Xiao, J. Chang, M. La Flèche and
	M.M. Abdelazim, M. Saediamiri and M. Birouk	M.I. Radulescu
	The Effects of Differential Diffusion on	Exportmental Study of Charle Elama
16:20 16:42	Turbulent Counter-flow Premixed Flames	Experimental Study of Shock-Flame
16:20-16:40	with Increasing Turbulence S.D. Salusbury,	Complex in a Hele-Shaw Cell M. La Flèche, Q. Xiao and M.I. Radulescu
	E. Abbasi-Atibeh and J.M. Bergthorson	Q. Лию ини 1v1.1. Кийинеэси

Wednesday May 17, 2017

8:00-8:10	Announcements	(McConnell 204)	
	Plenary Lecture 2 (McConnell 204): Thermodynamic and Optical Combustion		
	Characterization of Natural Gas Fuelling Strategies for Compression Ignition Engines		
8:10-9:00	Prof. Patrick Kirchen, Departm	nent of Mechanical Engineering	
	University Bri	tish Columbia	
	Chair: Gilles Bourque		
	McConnell 204	McConnell 11	
	Diagnostics	Detonations, explosions, and supersonic	
	Diagnootics	combustion	
	Chair: Adam M. Steinberg	Chair: Matei I. Radulescu	
	Simultaneous detection and partition		
	between soot and PAHs in a laminar		
	flame of methane by Single-Excitation	Single-head Detonation Propagation in a	
9:10-9:30	Wavelength TIme-REsolved Laser Induced	Partially Obstructed Square Channel	
	Incandescence and Fluorescence	M. Kellenberger and G. Ciccarelli	
	(SEW-TIRE LII/LIF) A. Hospital and		
	R. Lemaire		
	Approximating model error for	Near-limit detonations propagating in a	
	enhancement of soot morphology	medium with randomly distributed	
9:30-9:50	inference through multi-angle light	reactive sources X. Mi, A.J. Higgins,	
	scattering S. Talebi Moghaddam and	H.D. Ng, C.B. Kiyanda and N. Nikiforakis	
	K.J. Daun		
	Application of an In-Cylinder Line of		
	Sight Two-Colour Pyrometry Probe in an	Numerical Investigation of Flow Field	
9:50-10:10	Optical Pilot-Ignited Direct Injection	Inhomogeneities in a Rotating Detonation	
	Natural Gas Engine J. Yeo, M. Khosravi, J. Rochussen and P. Kirchen	Engine K.P. Grogan and M. Ihme	
	Development of a research-grade cylinder	Simultaneous inference of temperature	
	head with modular injector mounting and	and intensity scaling factor in	
10:10-10:30	access for multiple in-cylinder diagnostics	laser-induced incandescence T.A. Sipkens,	
	J. Rochussen, J. Son, J. Yeo, M. Khosravi and	R. Mansmann, J. Menser, K.J. Daun, T. Dreier	
	P. Kirchen	and C. Schulz	
10:30-10:50 Coffee break in McConnell 12			
	Laminar flames	Fire research	
	Chair: Patrick Kirchen	Chair: Larry W. Kostiuk	
	Impact of the numerical initial	Heat Flux Measurments During a	
10:50-11:10	pertubations and kinetic schemes on a	Full-Scale House Fire <i>M. Fulton</i> ,	
10.50-11.10	flame instability CFD model L. Le Corvec,	M. Fauchoux, D. Torvi and A. Beitel	
	D. Lapalme and P. Seers	111. 1 unchoux, D. 10101 unu 11. Deuti	

	Numerical and experimental study of	
	sooting propensity of ethanol in laminar	Extinguishing a flame with water droplets
11:10-11:30	diffusion flames at elevated pressures	M. Mosavati, R. Carriveau and D.S. Ting
	W. Syed, P.H. Joo, Ö.L. Gülder and C.P.T. Groth	
	Soot Particle Concentration Estimator	Numerical simulations of an
11:30-11:50	Applied to a Transient Sooting	underventilated compartment fire
11.30 11.30	Ethylene/air System L. Zimmer,	D.P. Wilson and C. Devaud
	R. Alexander and S.B. Dworkin	D.1. Wason and C. Deouau
	Numerical Investigation of Transfer	
	Function Models of a Laminar Premixed	The effect of wind shear and turbulence
11:50-12:10	Flame Using Frequency Response	on flame extinction J. Shen, R. Carriveau
	Analysis M. Sahafzadeh, L.W. Kostiuk and	and D.S. Ting
	S.B. Dworkin	
	Mechanism Reduction of Methane-Air	Comparison of Temperatures Measured
12:10-12:30	Flames Using Quasi Steady-State	During Sprinklered and Unsprinklered
	Approximation <i>A. Durocher, P. Versailles,</i>	Public Fire Demonstrations <i>M. Fulton,</i>
	J.M. Bergthorson and G. Bourque	M. Fauchoux, D. Torvi and A. Beitel
12:30-14:00	Lunch (On your own, see suggestion list)	
	McConnell 13	McConnell 11
	Heterogeneous and spray combustion	New technology concepts
	Heterogeneous and spray combustion Chair: Seth B. Dworkin	
	Heterogeneous and spray combustion Chair: Seth B. Dworkin A Microgravity Spaceflight Experiment to	New technology concepts Chair: Matthew R. Johnson
	Heterogeneous and spray combustion Chair: Seth B. Dworkin A Microgravity Spaceflight Experiment to Examine the Discrete Regime of Flame	New technology concepts Chair: Matthew R. Johnson Coupled simulations of partial oxidation
14:00-14:20	Heterogeneous and spray combustion Chair: Seth B. Dworkin A Microgravity Spaceflight Experiment to Examine the Discrete Regime of Flame Propagation: PERWAVES J. Palecka,	New technology concepts Chair: Matthew R. Johnson Coupled simulations of partial oxidation of methane in mixed ionic-electronic
14:00-14:20	Heterogeneous and spray combustion Chair: Seth B. Dworkin A Microgravity Spaceflight Experiment to Examine the Discrete Regime of Flame	New technology concepts Chair: Matthew R. Johnson Coupled simulations of partial oxidation
14:00-14:20	Heterogeneous and spray combustion Chair: Seth B. Dworkin A Microgravity Spaceflight Experiment to Examine the Discrete Regime of Flame Propagation: PERWAVES J. Palecka, S. Goroshin, J.M. Bergthorson and A.J. Higgins	New technology concepts Chair: Matthew R. Johnson Coupled simulations of partial oxidation of methane in mixed ionic-electronic conducting membrane reactors D. Sommer and P. Kirchen
14:00-14:20	Heterogeneous and spray combustionChair: Seth B. DworkinA Microgravity Spaceflight Experiment toExamine the Discrete Regime of FlamePropagation: PERWAVES J. Palecka,S. Goroshin, J.M. Bergthorson and A.J. HigginsSpherically-Expanding Flames in Hybrid	New technology conceptsChair: Matthew R. JohnsonCoupled simulations of partial oxidationof methane in mixed ionic-electronicconducting membrane reactors D. Sommerand P. KirchenHighly preheated premixed combustion
	Heterogeneous and spray combustion Chair: Seth B. DworkinA Microgravity Spaceflight Experiment to Examine the Discrete Regime of Flame Propagation: PERWAVES J. Palecka, S. Goroshin, J.M. Bergthorson and A.J. HigginsSpherically-Expanding Flames in Hybrid Aluminum-Methane-Oxidizer Mixtures	New technology concepts Chair: Matthew R. JohnsonCoupled simulations of partial oxidation of methane in mixed ionic-electronic conducting membrane reactors D. Sommer and P. KirchenHighly preheated premixed combustion for gas turbine applications
14:00-14:20	Heterogeneous and spray combustion Chair: Seth B. DworkinA Microgravity Spaceflight Experiment to Examine the Discrete Regime of Flame Propagation: PERWAVES J. Palecka, S. Goroshin, J.M. Bergthorson and A.J. HigginsSpherically-Expanding Flames in Hybrid Aluminum-Methane-Oxidizer Mixtures J.E. Vickery, P. Julien, S. Goroshin, D.L. Frost	New technology concepts Chair: Matthew R. JohnsonCoupled simulations of partial oxidation of methane in mixed ionic-electronic conducting membrane reactors D. Sommer and P. KirchenHighly preheated premixed combustion for gas turbine applications A. Landry-Blais, B. Picard, J. Dufault,
	Heterogeneous and spray combustion Chair: Seth B. DworkinA Microgravity Spaceflight Experiment to Examine the Discrete Regime of Flame Propagation: PERWAVES J. Palecka, S. Goroshin, J.M. Bergthorson and A.J. HigginsSpherically-Expanding Flames in Hybrid Aluminum-Methane-Oxidizer Mixtures	New technology concepts Chair: Matthew R. JohnsonCoupled simulations of partial oxidation of methane in mixed ionic-electronic conducting membrane reactors D. Sommer and P. KirchenHighly preheated premixed combustion for gas turbine applications A. Landry-Blais, B. Picard, J. Dufault, T. Parent-Simard, M. Charette, F. Ebacher,
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14:20-14:40	 Heterogeneous and spray combustion Chair: Seth B. Dworkin A Microgravity Spaceflight Experiment to Examine the Discrete Regime of Flame Propagation: PERWAVES J. Palecka, S. Goroshin, J.M. Bergthorson and A.J. Higgins Spherically-Expanding Flames in Hybrid Aluminum-Methane-Oxidizer Mixtures J.E. Vickery, P. Julien, S. Goroshin, D.L. Frost and J.M. Bergthorson Hypergolic droplet ignition of liquefying 	New technology concepts Chair: Matthew R. JohnsonCoupled simulations of partial oxidation of methane in mixed ionic-electronic conducting membrane reactors D. Sommer and P. KirchenHighly preheated premixed combustion for gas turbine applications A. Landry-Blais, B. Picard, J. Dufault, T. Parent-Simard, M. Charette, F. Ebacher, F. Marois and M. PicardDynamic Response of a Lean-Premixed Flame to Diffuse Non-Equilibrium
	 Heterogeneous and spray combustion Chair: Seth B. Dworkin A Microgravity Spaceflight Experiment to Examine the Discrete Regime of Flame Propagation: PERWAVES J. Palecka, S. Goroshin, J.M. Bergthorson and A.J. Higgins Spherically-Expanding Flames in Hybrid Aluminum-Methane-Oxidizer Mixtures J.E. Vickery, P. Julien, S. Goroshin, D.L. Frost and J.M. Bergthorson Hypergolic droplet ignition of liquefying hybrid rocket propellants with hydrides 	New technology concepts Chair: Matthew R. JohnsonCoupled simulations of partial oxidation of methane in mixed ionic-electronic conducting membrane reactors D. Sommer and P. KirchenHighly preheated premixed combustion for gas turbine applications A. Landry-Blais, B. Picard, J. Dufault, T. Parent-Simard, M. Charette, F. Ebacher, F. Marois and M. PicardDynamic Response of a Lean-Premixed Flame to Diffuse Non-Equilibrium Plasma at Atmospheric Pressure
14:20-14:40	 Heterogeneous and spray combustion Chair: Seth B. Dworkin A Microgravity Spaceflight Experiment to Examine the Discrete Regime of Flame Propagation: PERWAVES J. Palecka, S. Goroshin, J.M. Bergthorson and A.J. Higgins Spherically-Expanding Flames in Hybrid Aluminum-Methane-Oxidizer Mixtures J.E. Vickery, P. Julien, S. Goroshin, D.L. Frost and J.M. Bergthorson Hypergolic droplet ignition of liquefying 	New technology concepts Chair: Matthew R. JohnsonCoupled simulations of partial oxidation of methane in mixed ionic-electronic conducting membrane reactors D. Sommer and P. KirchenHighly preheated premixed combustion for gas turbine applications A. Landry-Blais, B. Picard, J. Dufault, T. Parent-Simard, M. Charette, F. Ebacher, F. Marois and M. PicardDynamic Response of a Lean-Premixed Flame to Diffuse Non-Equilibrium

15:00-15:20	Fabrication and characterization of magnetron sputtered Cu2O, Cu, and Al thermite nanolaminates L. LeSergent, J.Z. Wen and C. Ren	Characteristics of an Atmospheric Pressure Diffuse Nanosecond Pulsed Discharge for Methane Dissociation P. Diaz Gomez Maqueo, M. Maier, M.D.G. Evans, S. Coulombe and J.M. Bergthorson	
15:20-15:40	McConnell 13	McConnell 11	
	Turbulent flames		
	Chair: William L. Hallett		
	Numerical simulation of premixed		
	propane-air flame propagation in a		
15:40-16:00	straight rectangular duct using XiFoam		
	Z. Movahedi, I. Gallage and A. Sobiesiak		
	Locally Adaptive Tabulation of		
16:00-16:20	Low-Dimensional Manifolds using Bézier		
10.00-10.20	Patch Reconstruction M. Yao, M. Mortada,		
	C. Devaud and J. Hickey		
	Flamelet Modeling of Premixed		
	Methane-Hydrogen Fuel Combustion in		
16:20-16:40	an Multiple-Swirl Flame Configuration		
	S. Jella, J.M. Bergthorson, W.Y. Kwong and		
	A.M. Steinberg		
17:00-18:00	Annual Business Meeting of the Canadian Section (McConnell 204)		
18:00-18:30	Buses will start loading at 18:00, and the last one will leave at 18:30, for the sugar shack.		
	_	See map for the gathering point.	
19:00-21:30	Banquet at Érablière Charbonneau		
21:30-22:30	Buses return to McGill University		

Thursday May 18, 2017

8:00-8:10	Announcements	(McConnell 204)
Plenary Lecture 3 (McConnell 204): The deto		tonation paradox: the influence of diffusive
8:10-9:00	processes in controlling the	burning rate in detonations
-	Prof. Matei Ioan Petru Radulescu, D	epartment of Mechanical Engineering
		of Ottawa
	-	M. Bergthorson
	McConnell 204	McConnell 11
	Heterogeneous and spray combustion	Turbulent flames
	Chair: Madjid Birouk	Chair: Kyle J. Daun
9:10-9:30	Propagation Limits of Particulate Systems and Geometric Scaling <i>F. Lam, X. Mi and</i> <i>A.J. Higgins</i>	Application of inter-ensemble regularization to the CSE model for turbulence-chemistry interaction G.R. Hendra and W.K. Bushe
9:30-9:50	Evaluation of an Eulerian-Lagrangian Spray Atomization (ELSA) Model for Nozzle Flow: Modeling of Coupling Between Dense and Disperse Regions T.F. Leung, C.P.T. Groth and J.T.C. Hu	Validation of the assumptions underlying CSE using experimental data W.K. Bushe
9:50-10:10	A Fourteen-Moment Bi-Gaussian Closure for the Simulation of Disperse Liquid Fuel Sprays J. Laplante, C.P.T. Groth, F. Laurent and A. Vie	Lyapunov exponent as a metric to determine the quality and predictability of large-eddy simulations of turbulent combustion J. Labahn, G. Nastac, L. Magri and M. Ihme
10:10-10:30	Establishing Critical Design Parameters for the Optimization of Internally Mixed Air-Blast Nozzles for Pyrolysis Liquid Biofuels S. Albert-Green and M.J. Thomson	
10:30-10:50 Coffee break in McConnell 12		McConnell 12
	Pollutant formation Chair: Ömer L. Gülder	IC and gas-turbine engine combustion Chair: Andrzej Sobiesiak
10:50-11:10	Soot Concentration Estimation Using Lagrangian Post-Processing for Laminar Flames of Varying Dilution and Pressures <i>R. Alexander and S.B. Dworkin</i>	Investigating the effect of temperature on NOx sensor cross sensitivity to ammonia using a physics based model M. Aliramezani, K. Ebrahimi, C.R. Koch and R.E. Hayes

11:10-11:30	Dependence of soot particle size on pressure in methane-air diffusion flames determined by thermophoretic sampling at pressures up to 20 bar P.H. Joo, M. Christensen, E. Griffin, B. Gigone and Ö.L. Gülder	An experimental and numerical study of natural gas/diesel dual-fuel engine at low load: Effect of diesel fuel injection timing A. Yousefi, M. Birouk and H. Guo
11:30-11:50	The Effect of Sodium Chloride Additive on the Evolution of Particles in a Diffusion Flame A. Moallemi,M. Kazemimanesh, L.W. Kostiuk and J.S. Olfert	Effects of Karlovitz number on Localised Forced Ignition of Turbulent Combustible Mixtures: A DNS Study D. Patel
11:50-12:10	Exploratory Experiments of Effects of Water, Hydrochloric Acid, and Sodium Chloride Solutions on Lab-Scale Flare Emissions A.M. Jefferson and M.R. Johnson	Wood Pyrolysis Oil for Fueling Diesel Engine M. Khan, M. Rafiq, V. Sookarah and M.J. Thomson
12:10-12:30	Measurements of Benzene Destruction Efficiency in a Lab-Scale Flare N.T. Brooker, M.R. Johnson and B.M. Crosland	

Plenary Lecture: Tuesday May 16, 2017

Tailoring the Ignition and Combustion of Aluminum in Propellants

Steven F. Son

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Aluminum is used widely in solid propellants, and other energetic materials, because it yields significant impulse performance gains and improved stability at reasonable cost and good storage life. Generally, particle size and morphology are all that can be changed. Nanoscale metal fuels do offer potential advantages, including faster burning rates and more complete combustion. Motivated by this, replacing micrometer-scale aluminum in energetic materials with nanoscale aluminum has been studied for more than two decades, including studies involving aluminium-water propellants that will be reviewed in this talk. However, simply substituting micrometer-scale particles with nanoscale particles in solid propellants can lead to drawbacks including poor rheology and mechanical properties. Nanoscale aluminum also has a relatively thick oxide layer that reduces the performance. Indeed, examples of fielded propellants containing nanoscale aluminum are not currently found and may likely never be. A key question is how one can obtain the advantages of nanoscale fuels without the drawbacks. Recently, efforts have focused on micrometer-scale aluminum particles with an intraparticle nanoscale structure. The ideal solution may be a micrometer-sized composite particle that has significantly lower ignition temperature and, when ignited, produces much smaller particles/droplets. In multiphase liquid combustion, "micro-explosion" can occur for some miscible liquids and also in emulsions. A key requirement for this to occur is for one of the constituents to be more volatile than the others. For miscible liquids, a disparity between the liquid-phase mass and thermal diffusion is necessary in establishing droplet dynamics. Emulsions, such as fuel oils and water, can also yield self-atomization, or micro-explosion dynamics. In an analogy to liquid fuels, metal alloys are similar to miscible liquid fuels in that the atoms or molecules are mixed intimately to form a single phase, eutectic, or solid solution. Likewise, inclusions of more volatile materials within a metal fuel (e.g., a polymer in aluminum) are the equivalent to an emulsion where multiple phases are intertwined together, but not atomically or molecularly mixed. The intertwining of phases in a metal can be achieved using milling processes, which can result in lower particle ignition temperatures and dispersive dynamics. This method is also inexpensive and readily scalable. Another approach to achieve a similar outcome, which has also been pursued, could be the direct bottom-up fabrication of nanoscale fuel particles held together with a more volatile binder. In this talk I will review our efforts to tailor the ignition and combustion of aluminum in propellants. This has applications to other metals and other combustion systems. I will also discuss new directions that could allow even more tailoring of the combustion, including additive manufacturing applied to solid propellant fabrication.

Plenary Lecture: Wednesday May 17, 2017

Thermodynamic and Optical Combustion Characterization of Natural Gas Fuelling Strategies for Compression Ignition Engines

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In light of the significant North American natural gas (NG) reserves, NG is considered an attractive alternative fuel for internal combustion engines. Relative to combustion of diesel or gasoline, NG combustion results in lower CO_2 emissions, and potentially lower NO_x and particulate emissions. Beyond this, NG is often viewed as a transitional fuel, as technologies suitable for use with NG may be well suited for renewable natural gas (RNG), which is of particular interest for heavy-duty and large-bore engine applications, where alternative such as electrification are not as attractive for de-carbonization. While NG is an attractive alternative fuel, it is nonetheless plagued by significant methane emissions, which can account for a significant increase in greenhouse gas emissions. In the case of spark ignited engines, NG requires high ignition energies, particularly for lean operation, resulting in limited spark plug life. For heavy duty applications, compression ignition NG fuelling strategies are preferred due to their higher efficiencies and improved ignition robustness, relative to spark ignited approaches.

In this work, two NG compression ignition fuelling approaches are considered. In both approaches, the combustion of a second fuel, such as conventional diesel, is used for the ignition of the NG. In "dual-fuel" strategies, a premixed air-NG mixture is compressed and ignited near top dead center by the combustion of a small, direct-injected diesel "pilot". Depending on the relative quantities of air, premixed NG, and direct-injected diesel, as well as the diesel pilot injection pressure, the fuel conversion efficiency and emissions can vary significantly. High Pressure Direct Injection (HPDI) of NG provides an alternative dual fuel strategy with the potential for significantly lower methane emissions and higher efficiency. During HPDI operation, NG is injected directly into the combustion chamber when the piston is near top dead center. Similar to premixed dual fuel combustion, a small diesel pilot combustion event is used to ignite the NG, resulting in a mixing controlled combustion process. Due to the non-premixed nature of HPDI combustion, higher compression ratios and fuel conversion efficiencies are possible, as are lower methane emissions.

A convertible thermodynamic (*i.e.*, metal) and optical single cylinder engine is used here to characterize the combustion and emissions performance of premixed dual fuel and HPDI combustion strategies. Of particular interest is the effect of fuelling parameters on the combustion mode, which was observed to include (partially) premixed flame propagation, multipoint autoignition, and/or mixing controlled combustion, depending on the fuelling approach. For premixed dual-fuel combustion, regimes of flamepropagation and non-flame-propagation were identified on the basis of heat release rate characteristics and high-speed OH* chemiluminescence imaging. The fuelling conditions resulting in these combustion modes are identified using an equivalence ratio - diesel substitution rate map. In addition, the sensitivity of the reaction zone evolution (ignition, propagation, and growth) to the pilot injection pressure is demonstrated through the use of OH* chemiluminescence and visible luminosity imaging. A preliminary characterization of HPDI combustion was also carried out to identify the influences of injection parameters (injection pressure, relative NG and diesel injection timings) on the combustion process. Due to the large size and high-pressure fuel supply requirements of the HPDI injector, a new cylinder head was developed to accommodate the HPDI injector, and additionally included accesses for in-cylinder diagnostics. Here, this access was used for pyrometric and infrared absorption probes to characterize the local in-cylinder particulate matter concentration and temperature, and methane concentration, respectively. Through this preliminary characterization, high-speed OH* and natural luminosity imaging were used to provide the first in-cylinder optical characterization of HPDI NG combustion.

Plenary Lecture: Thursday May 18, 2017

The detonation paradox: the influence of diffusive processes in controlling the burning rate in detonations

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Traditionally, detonation waves have been assumed as being governed by the reactive inviscid Euler equations. Transport phenomena, which govern the propagation of low-speed reactive waves (flames) are neglected. In recent years, with the growth in the numerical resources available, Euler simulations have been possible with high resolution. These results have demonstrated a fundamental paradox when compared to experiments. While experiments have demonstrated that more unstable detonations can be initiated easier and are more difficult to fail, the predictions based on the Euler equations have shown clearly the opposite trend. The paradox is not unlike the well-known d'Alembert paradox in fluid mechanics, whereby inviscid potential flow fails to capture the experimentally observed drag forces on an object.

My talk will highlight the physics of unstable turbulent detonation waves for which diffusive phenomena (amplified by turbulence) control the burning rate of gases inside the reaction zone structure of detonations. Due to the inherent cellular instability of detonations, the stronger shocks provide auto-ignition events, while the weaker shocks give rise to unburned pockets. These are surrounded by reactive gas in what resembles a distributed regime of turbulent combustion. These pockets burn out by surface turbulent flames.

I review detailed experiments of the detonation structure, which reveal the main mechanisms promoting turbulent mixing: Kelvin-Helmholtz on shear layers, Richtmyer-Meshkov from shock-flame interactions and internal strong jet formation associated with shock reflections.

The paradox identified points to the necessity of modeling not only the detonation instability, which provides the driving mechanism of turbulence, but also the dissipation of turbulence, which controls the reaction rate of approximately half the gas processed by the detonation front.

Given the unique character of detonation waves, which require a proper description of turbulent flame propagation by transport, auto-ignition phenomena and gas dynamics, typical tools used in LES of turbulent combustion (*e.g.*, flamelet or thickened flame approaches) are not possible. I highlight our recently demonstrated computational methodology for detonations based on the Linear Eddy Model for turbulent combustion and its extensions to compressible flow in the context of Large Eddy Simulations.